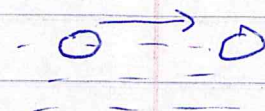


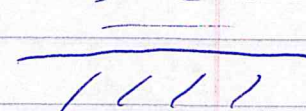
Chapter 3 Properties of fluids

move from $\downarrow$ to $\downarrow$
 $\rightarrow$ 

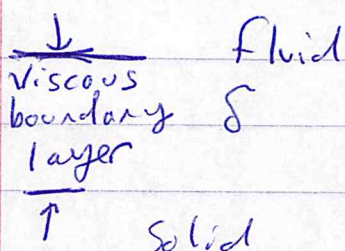


Fluid 

Applying a stress
 causes the fluid parcel
 to relocate,

Solid 

applying a stress
 the solid moves
 but will restore
 to original position
 when released


 viscous
 boundary
 layer δ
 fluid
 solid



$z \uparrow$ $x \rightarrow$ $U(x, z)$

oscillating boundary, $f = \text{frequency}$
Boundary Condition: No slip of fluid solid-
 boundary at interface.

$$\delta = \left(\frac{2\eta}{\rho\omega} \right)^{1/2}$$

$$\omega = 2\pi f$$

One definition of
 viscosity η

For air

$$\eta = 1.98 \times 10^{-5} \frac{\text{kg}}{\text{m s}} \left[\frac{\text{Pa s}}{\text{Pa s}} \right] \text{Pa} = \frac{\text{kg}}{\text{m s}^2} = \frac{\text{Force}}{\text{Area}}$$

Roughly $\eta(T) \propto T^{1/2}$

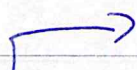
Form of a transport

Example: Air @ 300K $\rho = 1 \text{ kg/m}^3$

(air)
Length over which a fluid supports
velocity shear as a function of frequency

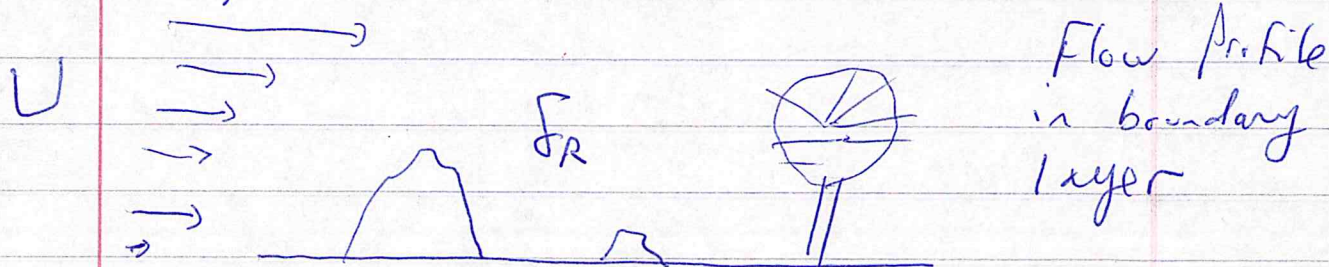
Pg 3.2

f (Hz)	δ (meters)	
0.01	2.5×10^{-2}	2.5 cm
0.1	7.9×10^{-3}	8 mm
1	2.5×10^{-3}	2.5 mm
10	0.8 mm	
100	0.25 mm	
1000	79 μ m	



Sound frequencies in atmosphere,
Smooth boundaries interact only with
over about 1 hair width away. Many
Surfaces are not smooth on an 80 μ m
length scale.

Analogy



δ_R = Surface roughness scale
 ~ 1 to 100 meters land
 ~ 0.1 to 10 meters ocean.

Flow dragged, blocked, and redirected by
Surface roughness elements.

Not Covered

Midlatitude Atmos

Pg 3.3

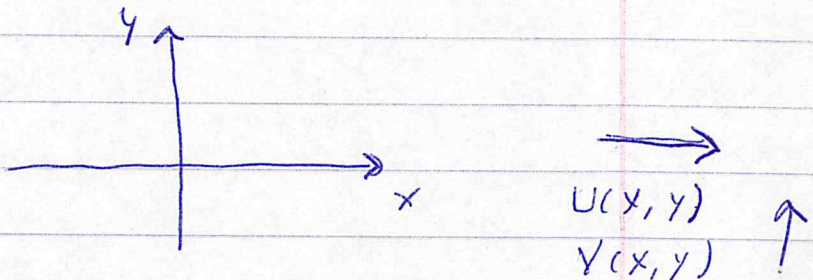
Covered in
Ch2 of Lynch with my Problem

§ 1.4 Basic Kinematics of Fluids from

Mid latitude atmospheric dynamics by Jonathan Martin, [very good general description and introduction of Vorticity and divergence]

Take a 2-D Fluid Problem:

Need fluid equations to see how they come about



Consider slight perturbations of the fluids:

$$(1) \quad U(x, y) = U_0 + \left. \frac{\partial U}{\partial x} \right|_0 x + \left. \frac{\partial U}{\partial y} \right|_0 y + \text{H.O.T.}$$

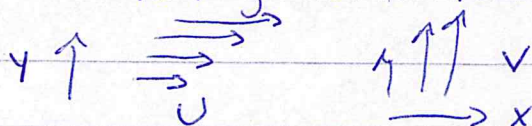
$$(2) \quad V(x, y) = V_0 + \left. \frac{\partial V}{\partial x} \right|_0 x + \left. \frac{\partial V}{\partial y} \right|_0 y + \text{H.O.T.}$$

Define: $D \equiv \text{divergence} = \frac{\partial U}{\partial x} + \frac{\partial V}{\partial y}$

$$F_1 \equiv \text{Stretching deformation} = \frac{\partial U}{\partial x} - \frac{\partial V}{\partial y}$$

[Positive definite if U gets larger along x , V smaller along y]

$$F_2 = \text{Shearing deformation} = \frac{\partial U}{\partial y} + \frac{\partial V}{\partial x}$$



$$\zeta \equiv \text{Vorticity} \equiv \frac{\partial V}{\partial x} - \frac{\partial U}{\partial y} \quad \text{Extremely important}$$

Not Covered

Cont

Pg 3.4

Using definitions and algebra,

Perturbation of U and V

$$\tilde{U} \equiv U(x,y) - U_0 = \frac{1}{2} (D_x + F_1 x - \zeta y + F_2 y)$$
$$\tilde{V} \equiv V(x,y) - V_0 = \frac{1}{2} (\zeta x + F_2 x + D_y - F_1 y)$$

Now we can study each in isolation:

§ 1.4.1 Pure Vorticity; Set $\zeta = 1$
 $F_1, F_2, D = 0$

$$\tilde{U} = -\frac{1}{2} y$$

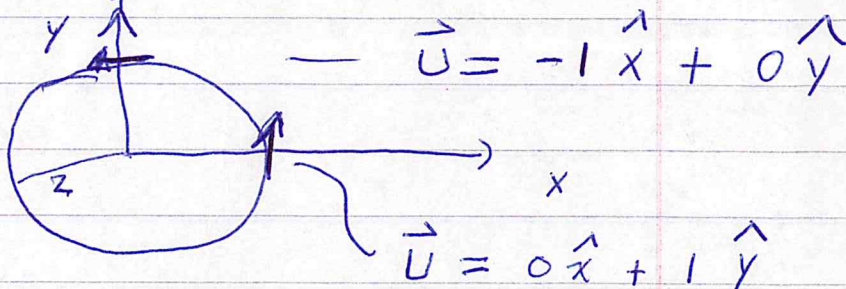
$$\vec{U} = \tilde{U} \hat{x} + \tilde{V} \hat{y}$$

$$\tilde{V} = \frac{1}{2} x$$

To graph, choose a contour $\sqrt{\tilde{U}^2 + \tilde{V}^2} = 1$
(wind speed = 1)

$$\frac{x^2}{4} + \frac{y^2}{1} = 1$$

$$x^2 + y^2 = 2^2$$



Positive Vorticity has flow in ccw direction

Not
Covered

Pg 3.5

Cont

§ 1.4.2

Pure divergence

Let $D = 1$, $\mathcal{F}$, $F_1, F_2 = 0$

$$\begin{aligned}\tilde{U} &= \frac{1}{2}x &= \frac{dx}{dt} \\ \tilde{V} &= \frac{1}{2}y &= \frac{dy}{dt}\end{aligned}\left. \begin{array}{l} \\ \\ \end{array} \right\} \begin{array}{l} \text{Position} \\ \text{Change} \\ \text{with} \\ \text{time} \end{array}$$

Fluid flow is a function of x and y .
[From x_0, y_0, t_0 to x, y, t]

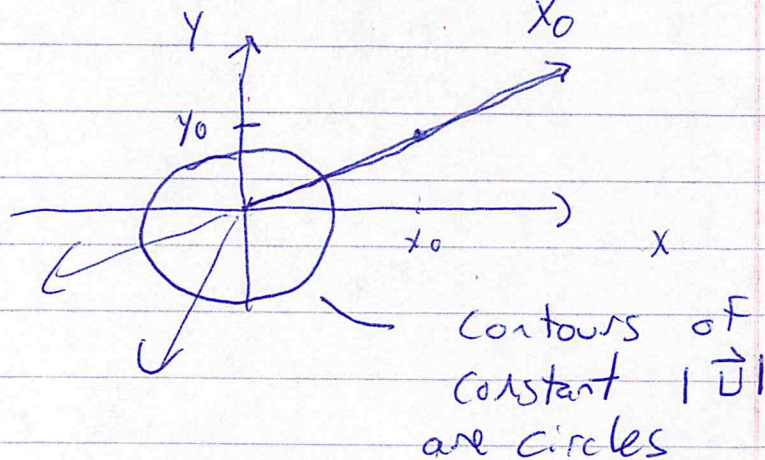
Calculate Pathlines of fluid [trajectory analysis]

$$\frac{dx}{dt} = \frac{x}{2} \quad \int_{x_0}^x \frac{dx'}{x'} = \frac{1}{2} \int_{t_0}^t dt'$$

$$\ln \frac{x}{x_0} = \frac{t-t_0}{2} = \ln \frac{y}{y_0}$$

Path lines are $y = \frac{y_0}{x_0} x$

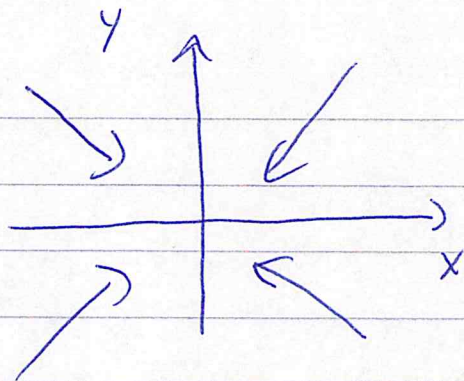
Fluid
diverges
from the
center



Not Covered

Cont

Pg 3.6



For $D=1$
get fluid

Convergence
towards
Center

[Need to have conservation equations, mass, energy, etc, to show how we can physically have D and S in a fluid]

Pure Stretching § 1.4.3

$$F_1 = 1$$

$$D, S, F_2 = 0$$

$$\tilde{U} = \frac{1}{2} x = dx/dt$$

$$\tilde{V} = -\frac{1}{2} y = dy/dt$$

Path lines

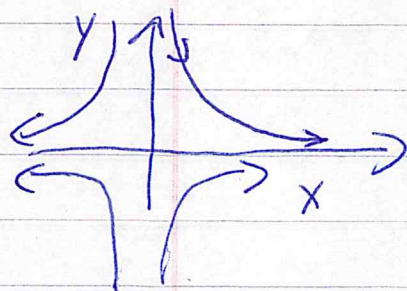
$$\frac{dx}{x} = \frac{dt}{2}$$

$$x = x_0 e^{(t-t_0)/2}$$

$$\frac{dy}{y} = -\frac{dt}{2}$$

$$y = y_0 e^{-(t-t_0)/2}$$

$$\Rightarrow y = \frac{x_0 y_0}{x}$$

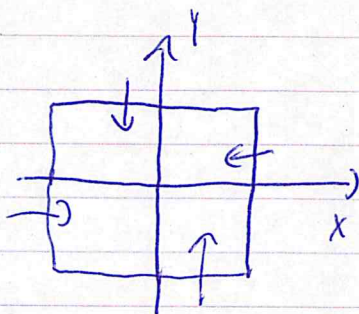


Not Covered

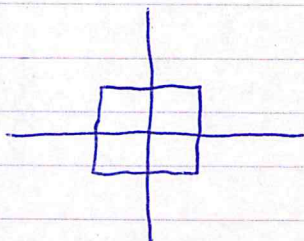
Cont

Pg 3.7

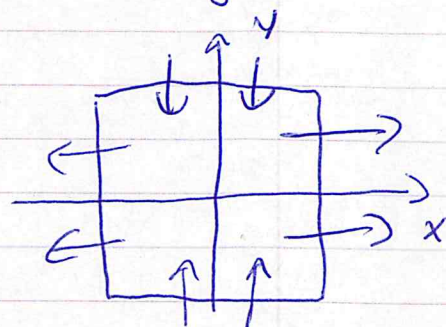
Divergence (convergence) Versus
Stretching (contracting)



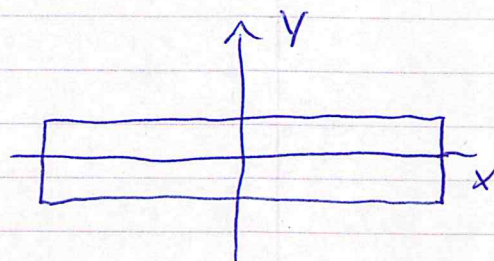
Convergence



(Box gets smaller)



Stretching

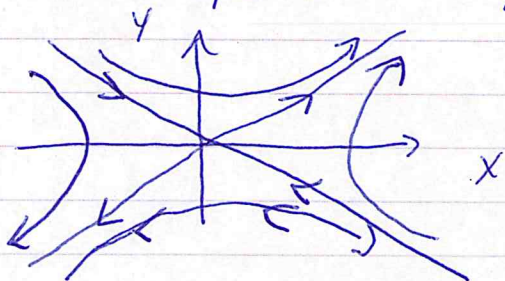


[Box turns into rectangle]

§ 1.4.4 Pure shearing deformation
 $F_2 = 1$

$$\tilde{U} = \frac{1}{2} y \quad \tilde{V} = \frac{1}{2} x$$

Pathlines are hyperbolic $y^2 - x^2 = y_0^2 - x_0^2$



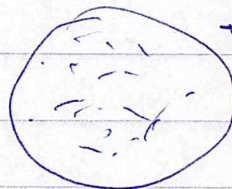
Different
Pathlines
for different
choices of
 x_0, y_0

§ 3.3.1 Dry atmosphere - adiabatic lapse rate.

Dry Air is 78% N_2 21% O_2 1% other - CO_2 , Ar, etc

Ideal Gas Law:

P = Pressure



V = volume

N = # molecules

T = Temperature

Point like billiard balls bouncing around

$$PV = NkT$$

$$k = 1.38 \times 10^{-23} \text{ J/molecule}^\circ K$$

$$\Rightarrow PV = (N_{N_2} + N_{O_2} + N_{CO_2} + N_{Ar} + \dots) kT$$

$$P = \underbrace{\frac{N}{V} \frac{\rho \text{ Kg mole}}{\text{mole } N_A \text{ molecules}}}_{\rho} \underbrace{\frac{N_A k}{N}}_{R_d} T$$

ρ = density

N_A = Avogadro's #

$$\rho = 29 \frac{\text{Kg}}{\text{mole}}$$

molecular weight
dry air

$$P = \rho R_d T$$

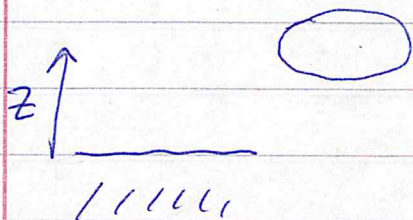
$$R_d = 287 \frac{\text{J}}{\text{Kg}^\circ K}$$

Fundamental
form
of
Ideal
Gas
Law
Partial
Pressure

$$\Gamma_0 = -dT/dz = g/c_p$$

Ag 3.9

Adiabatic Lapse Rate



Air Parcel created here

$$P, V, T, N, m = \frac{N \mu}{N_A}$$

(fixed $\frac{N \mu}{N_A}$)

E

$$H(z) = \underbrace{\frac{5}{2} k T N}_{\text{internal Energy [K.E.]}} + \underbrace{mgz}_{\text{P.E.}} + \underbrace{PV}_{\text{Work needed to "blow up" the parcel to Volume V against the pressure P of the surroundings.}}$$

Enthalpy

$$H \equiv E + PV$$

$$dH = dE + PdV + VdP$$

$$dE = dQ - PdV$$

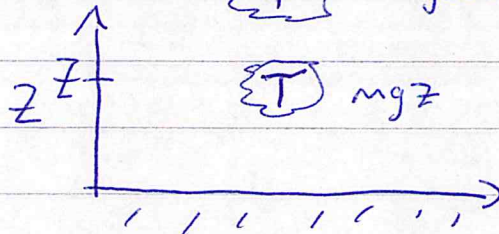
$$dH = dQ + VdP$$

Processes at constant P involve only heat transfer dQ

5 Energy Pathways in Equilibrium with each other at temperature T

$$\frac{1}{2} m (v_x^2 + v_y^2 + v_z^2) + \frac{1}{2} I (\omega_x^2 + \omega_y^2 + \omega_z^2)$$

$$z + dz - mg(z + dz)$$



Parcel Neutrally Stable if

$$H(z+dz) = H(z)$$

$$PV + PdV + VdP$$

$$\frac{5}{2} N k T + \frac{5}{2} N k dT + mgz + mgdz + (P + dP)(V + dV)$$

$$= \frac{5}{2} N k T + mgz + PV$$

pg 3.10

$$\frac{5}{2} N k dT + \frac{pN}{N_A} g dz + P dV + V dP = 0$$

↑
I. G. L.

Multiply by $\frac{N_A}{pN}$

$$P V = N k T$$

$$P dV + V dP = N k dT$$

$$\frac{5}{2} \frac{N_A k}{p} dT + g dz = 0$$

$$C_p = \frac{5}{2} R$$

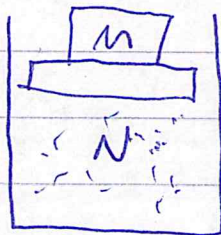
Specific heat at
Constant Pressure

$$\frac{dT}{dz} = -\frac{g}{C_p} = -\frac{p}{\rho}$$

$$C_p = 1004 \frac{\text{J}}{\text{kg} \cdot \text{K}}$$

Aside

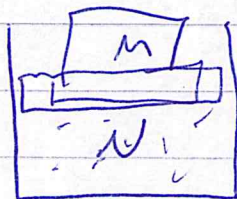
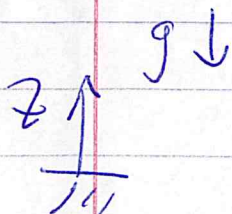
Definition of C_p



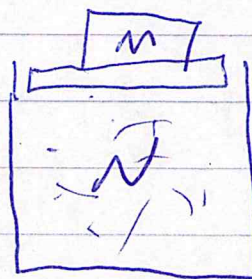
Frictionless Cup

$$\frac{N_A}{N_A} C_p \Delta T = Q$$

↑ Q heat in



T
Before



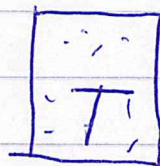
T + ΔT
after
Q applied

Some Q
needed to
raise mass
m up,
Some goes to
T increase.

By Contrast

 $V =$
constant

Before



After

T

greater
than
constant
pressure
process

$$\frac{N}{N_c} C_v \Delta T = Q$$

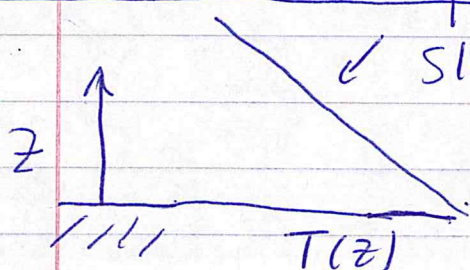
$$C_v = \frac{5}{2} R_d$$

$$C_p - C_v = R_d$$

$PV^\gamma = \text{constant}$
for a gas, adiabatic process

$$\gamma = C_p / C_v = 7/5 = 1.4$$

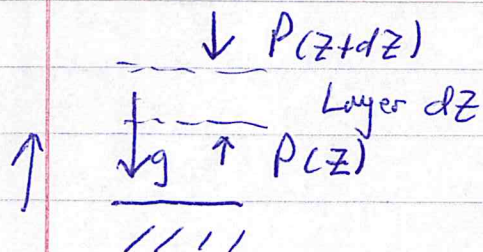
for dry air



Potential Temperature

Surface, $z=0$ $P = 1013.25 \text{ mb}$
 $\equiv P_0$

$$\frac{dT}{dz} = -\frac{g}{C_p} \Rightarrow T(z) = T_0 - \frac{g}{C_p} z$$

Force Balance
Hydrostatic Equilibrium

$$(\rho A dz)g + P(z+dz)A =$$

Layer mass

$$P(z)A$$

$$P(z+dz) \approx P(z) + \left(\frac{\partial P}{\partial z}\right) dz$$

$$= P(z) + dP$$

So

$$\boxed{\rho g dz = -dP}$$

 $dP = -\rho g dz$
Hydrostatic
Equation

$$\boxed{\frac{dP}{\rho} = -g dz}$$

So for

$$\frac{dT}{dz} = \frac{-g}{C_p}$$

$$C_p dT = -g dz = \frac{dP}{\rho}$$

For the ideal gas

$$P = \rho R_d T$$

$$\rho = \frac{P}{R_d T}$$

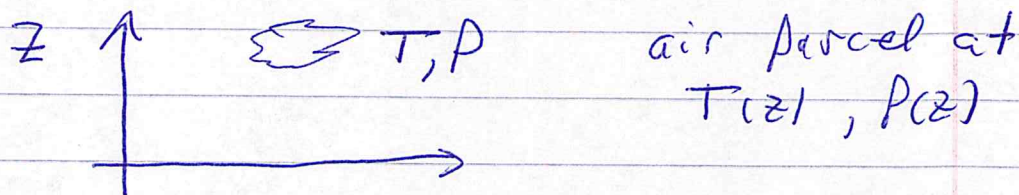
$$\text{Then } \int_{P_0}^P \frac{dP}{P} = \frac{C_p}{R_d} \int_{T_0}^T \frac{dT}{T}$$

← definition
of
Potential T_0

$$\ln \frac{P}{P_0} = \frac{C_p}{R_d} \ln \frac{T}{T_0}$$

T where $P = P_0 =$ Sea Level

$$T_0 = T \left(\frac{P_0}{P}\right)^{R_d/C_p}$$

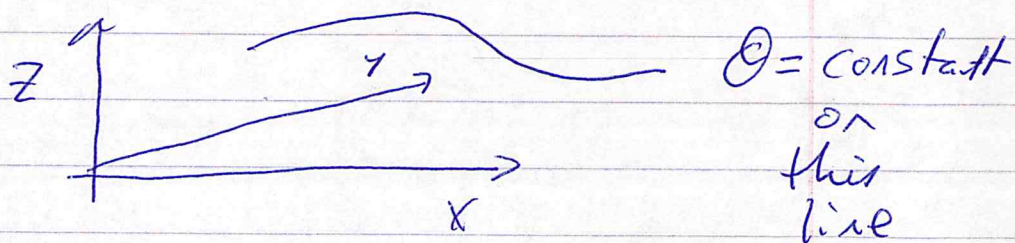
Summarizing:

If lowered adiabatically to $z=0$ sea level where $P(z=0) = P_0$, then

$$T(z=0) = \Theta = T \left(\frac{P_0}{P} \right)^{R_d/c_p}$$

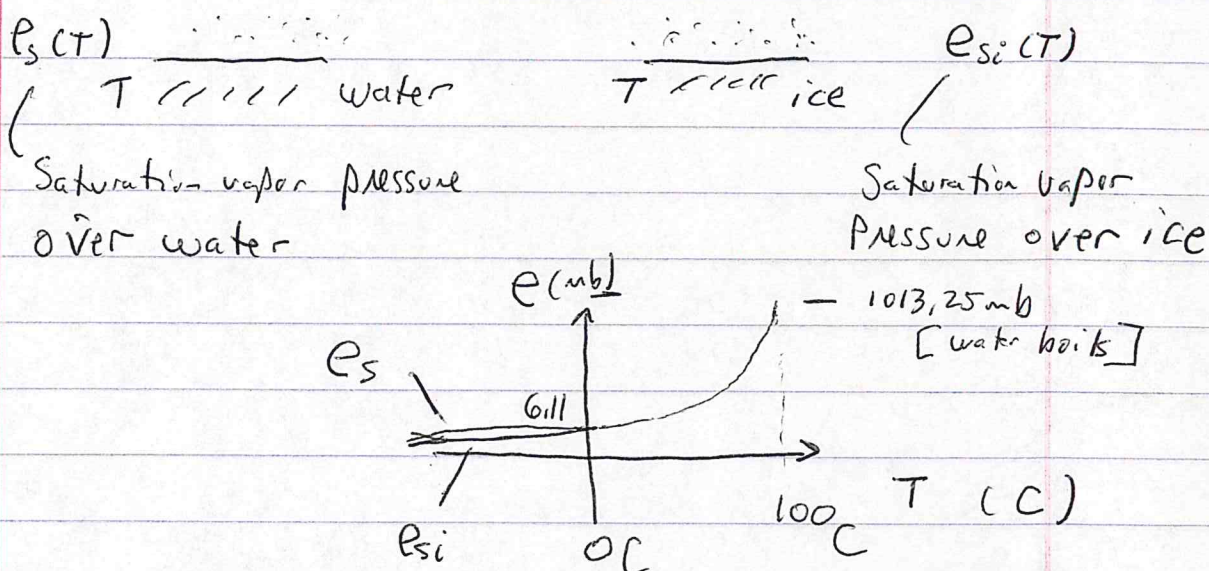
where $\frac{R_d}{c_p} = \frac{2}{7}$

Important because atmosphere is close to adiabatic at times;

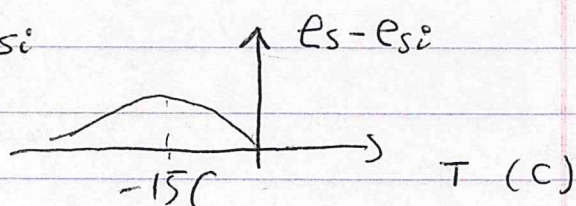


Line of contour of constant Θ is known as isentrope $\Rightarrow$ no heat needed to be added to have air parcels have the same entropy $\Rightarrow$ winds tend to follow isentropes. Entropy quantifies heat added to systems.

3.3.2 Moist atmosphere



Note: $e_s \geq e_{si}$



So at -15°C
 Super cooled droplets → ice crystals grow at the expense of water droplets.

[Known as the Wegener - Bergeron Findeisen Process]

If # of ice nuclei $\ll$ # cloud droplets $\Rightarrow$
 ice will grow large enough to fall out.

For dry air: $P = \rho R_d T$

For moist air we must add in the number of water vapor molecules per unit volume.

$$R_d = R \left[\frac{\text{J}}{\text{mole K}} \right] \frac{1000 \text{ moles}}{29 \text{ Kg}} \quad \left[\begin{array}{l} \text{Gas constant for} \\ \text{dry air} \end{array} \right]$$

$$R_v = R^* \times \frac{1000}{18} \frac{\text{J}}{\text{Kg}^\circ\text{K}} \quad \left[\begin{array}{l} \text{Gas constant for} \\ \text{water vapor} \end{array} \right]$$

Moist air:

(1)

$$P = (\rho_d R_d + \rho_v R_v) T$$

where

$$\rho = \rho_d + \rho_v$$

└ dry air └ water vapor

Define:

$$\frac{i}{q} = \frac{1}{w} + 1$$

$$q \equiv \rho_v / \rho \quad 1 - q = \rho_d / \rho$$

└ specific humidity

Note:

$$W \equiv \text{water vapor mixing ratio} = \frac{\rho_v}{\rho_d} \quad \text{so}$$

[g/Kg] typical

$W > q$ by a few percent at most.

Algebraically,

$W \approx q$

$$\frac{R_v}{R_d} = \frac{\rho_d}{\rho_v}$$

$$P = \rho R_d \left[(1 - q) + q R_v / R_d \right] T$$

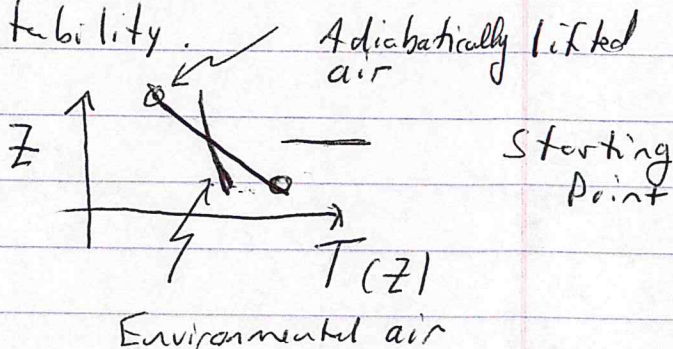
virtual temperature T_v definition

$$T_v \geq T. \quad \rho \text{ moist air} \leq \rho_{\text{dry}} \text{ at same } P \text{ \& } T$$

§ 3.4 Static Stability.

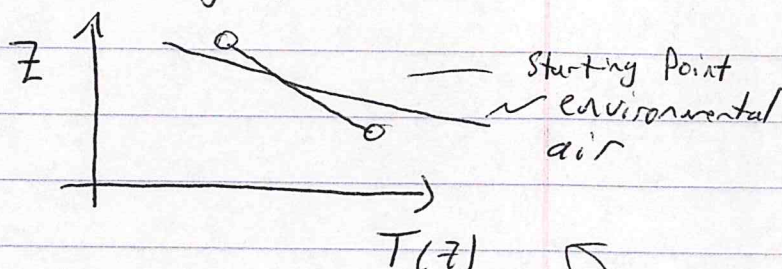
Key message:

Stable



Lifting [lowering] a parcel from starting point makes it cooler [warmer] than the environmental air at the same level, so the air would return, and maybe oscillate, about the starting point.

Unstable



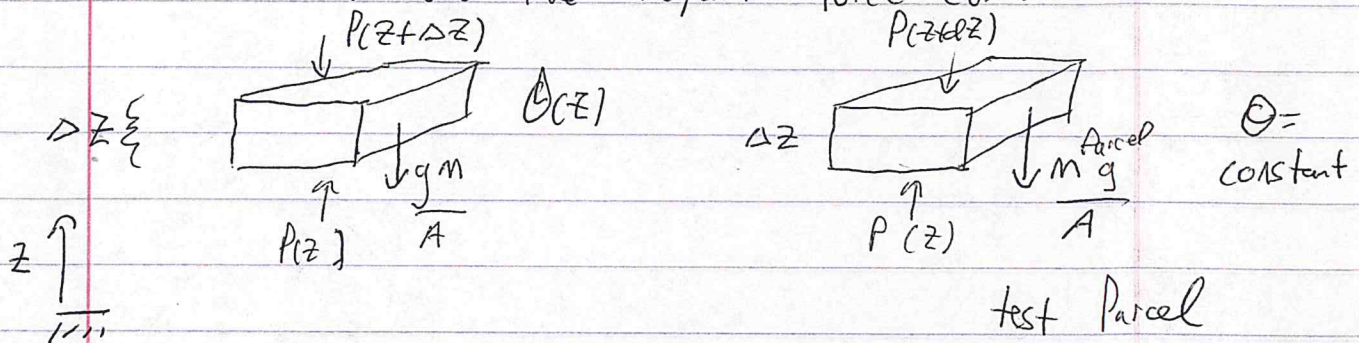
Near the midday solar heated surface this profile happens the lifted air is now warmer than surroundings so is less dense, so it rises up!

If the air is at saturation, lifting occurs along a moist adiabat.

[will do a section of skew T log P to illustrate phenomena at end of chapter]

Archimedes Principle:

Where does the buoyant force come from?



Environment:

$$\frac{\vec{F}_{\text{force}}}{A_{\text{area}}} = \hat{z} \left[\overbrace{P(z) - P(z+\Delta z)} - \int_z^{z+\Delta z} \rho(z') g dz' \right]$$

 $= 0$ For hydrostatic equilibrium

Test Parcel: $\frac{\vec{F}_{\text{force}}}{A_{\text{area}}} = \hat{z} \left[\underbrace{P(z) - P(z+\Delta z)} - \int_z^{z+\Delta z} \rho^{\text{parcel}}(z') g dz' \right]$

[We lift Somehow]

$$\approx \hat{z} (\rho(z+\Delta z) - \rho^{\text{parcel}}(z+\Delta z)) g \Delta z$$

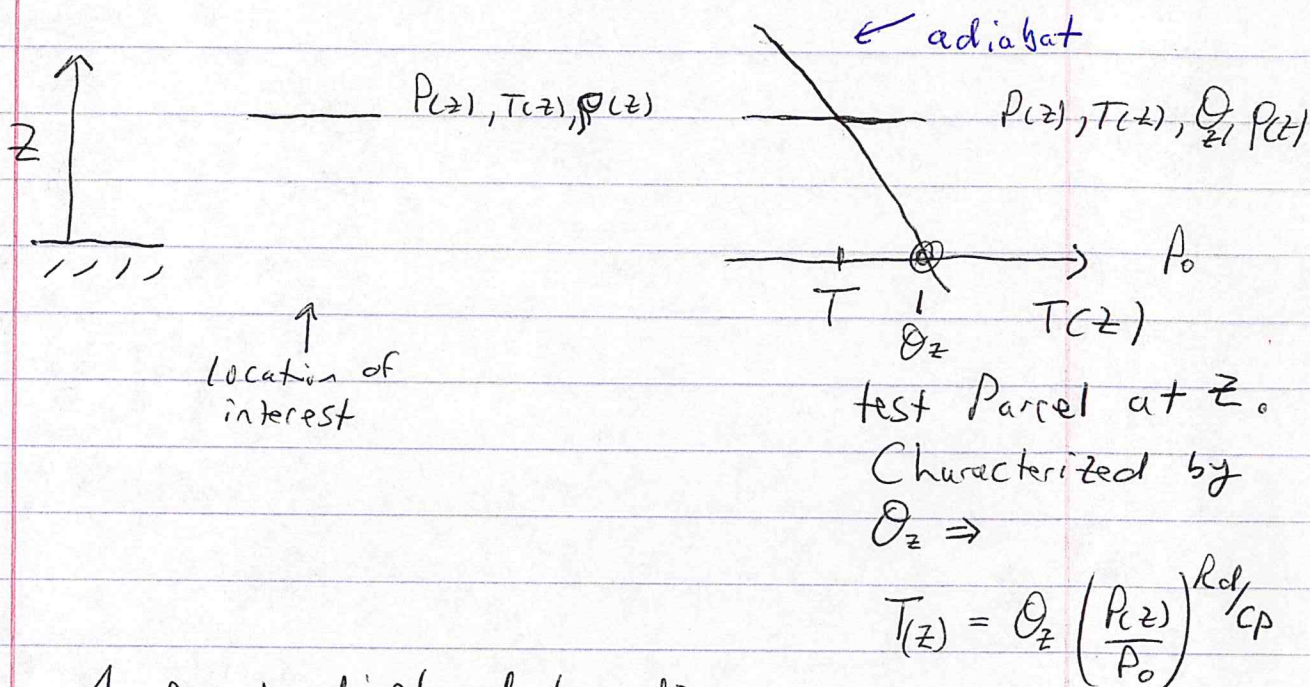
if Parcel is more dense [colder] $\vec{F} < 0$

So Parcel restores to original position.

[Another look at parcel theory]

Brunt - Väisälä frequency :

Very useful to understand gravity waves in the atmosphere — in the lee of mountains.



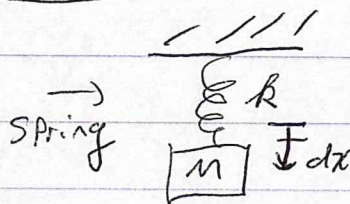
A parcel displaced by dz has a buoyant force acting on it. Acceleration is

$$\frac{1}{\theta} \frac{d\theta}{dz} = \frac{d \ln \theta}{dz}$$

$$\ddot{z} = - \underbrace{\frac{g}{\theta(z)} \frac{d\theta(z)}{dz}}_{N^2} dz = -N^2 dz$$

Analogous Problem

Could do first



$$F = m \ddot{x} = -kx$$

$$\ddot{x} = -\frac{k}{m} x$$

$$x = A e^{i\omega t}$$

$$\ddot{x} = -\omega^2 x$$

Resonance Frequency

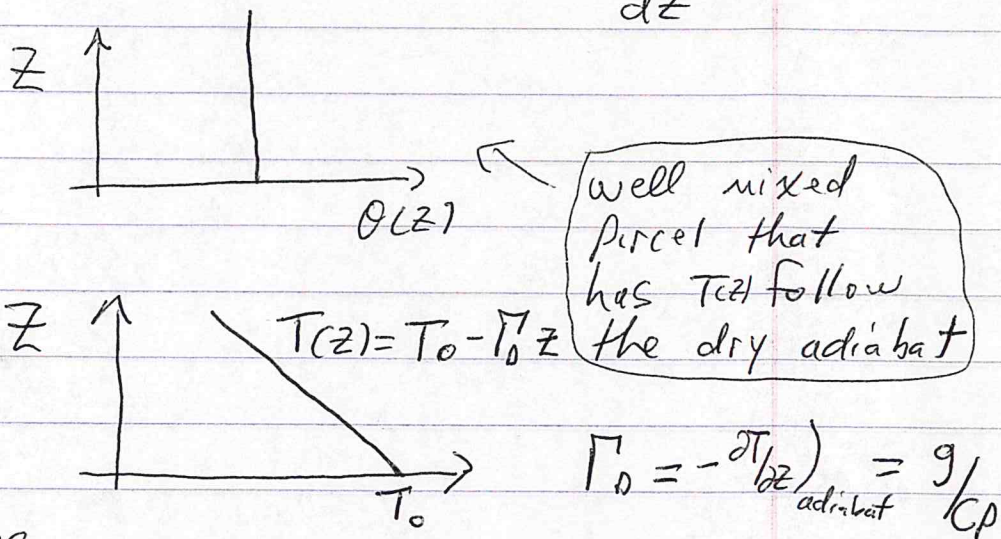
$$x = A \cos \omega t$$

$$\ddot{x} = -\omega^2 x$$

$$\rightarrow \omega = \sqrt{\frac{k}{m}}$$

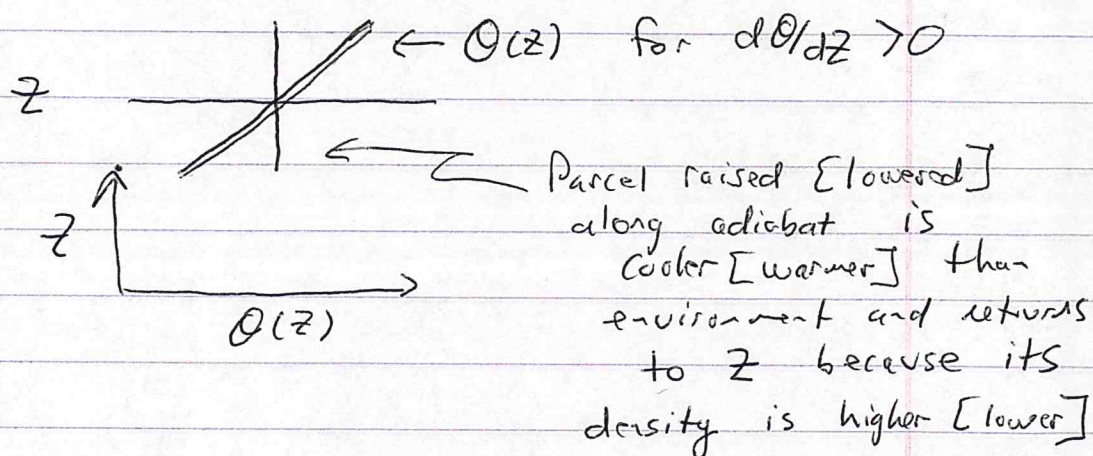
Ag 3.18

Case 1. $\theta(z) = \text{constant}$ $\frac{d\theta}{dz} = 0$



$\ddot{z} = 0$ in this case.

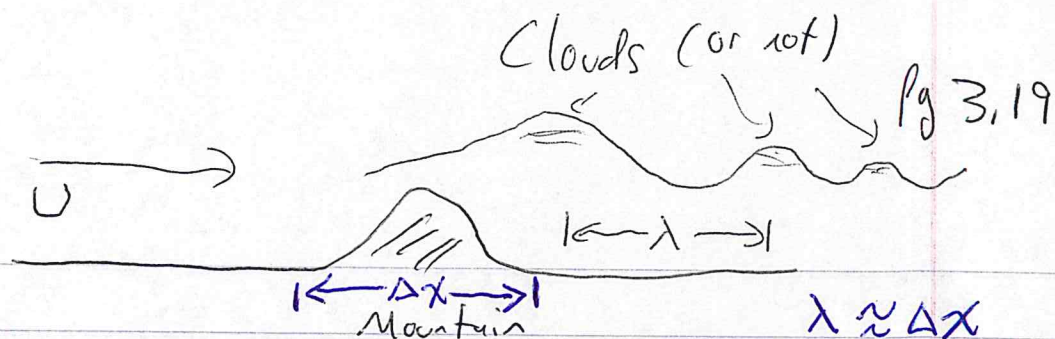
Case 2: $\frac{d\theta}{dz} > 0$ $N^2 = \frac{g}{\theta(z)} \frac{d\theta(z)}{dz} > 0$



$$\ddot{z} = -N^2 z \quad z = A \cos \omega t \quad \omega = N$$

More stable parcels have larger $\frac{d\theta}{dz}$, larger N ,

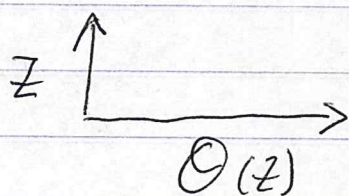
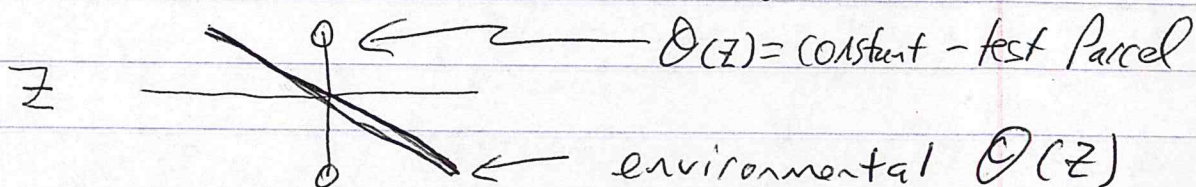
So oscillate faster, $\ddot{z} = -\omega A \cos \omega t = -N A \cos \omega t$ than less stable parcels.



Mountain waves have standing wave patterns where $\lambda \approx \frac{2\pi U}{N}$. Large N create small λ .

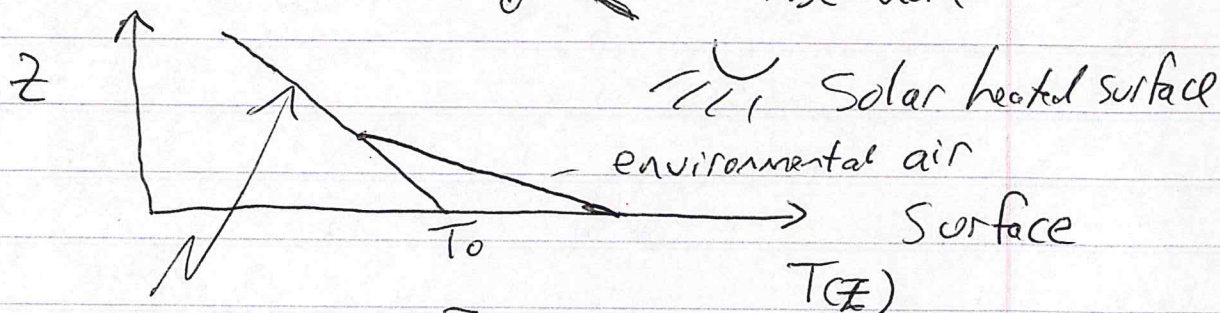
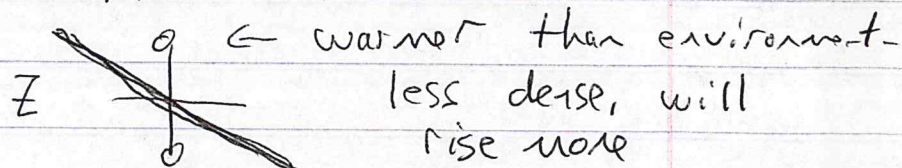
Often visible in satellite imagery.

Case 3: $\frac{d\theta}{dz} < 0$ $N^2 = \frac{g}{\theta} \frac{d\theta}{dz} < 0$



Unstable growth initial $\ddot{z} = |N|^2 z$
 $\ddot{z} = |N|^2 z$

Now a parcel raised above z will be unstable $\Rightarrow$ will continue to rise



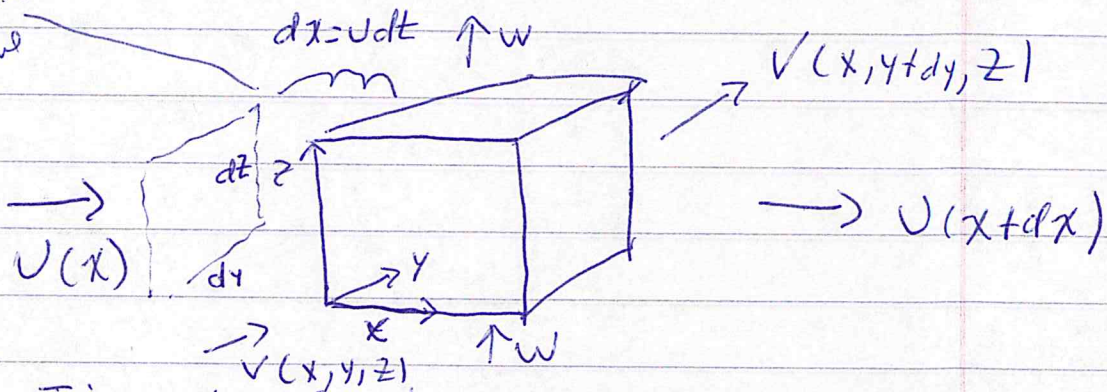
$T(z) = T_0 - \Gamma_0 z$
 $\theta(z) = T_0 = \text{constant}$

Continuity Equation for Mass Conservation of Mass

Fig 3.20

Small Cube

Mass in this volume cube in time Δt enters



Time rate of Change of mass in volume

$$\frac{dM}{dt} = \frac{\partial}{\partial t} \rho(x, y, z) dx dy dz =$$

Rate of mass in - rate of mass out

$$= \rho U(x) dy dz - \rho U(x+dx, y, z) dy dz + \rho V dx dz - \rho V(y+dy) dx dz + \rho W dx dy - \rho W(z+dz) dx dy \quad (1)$$

$$\rho U(x+dx, y, z) \approx \rho U(x, y, z) + \frac{\partial \rho U}{\partial x} dx$$

Same for V and W.

(1) becomes

$$- \frac{\partial}{\partial x} \rho U dx dy dz - \frac{\partial}{\partial y} \rho V dx dy dz - \frac{\partial}{\partial z} \rho W dx dy dz$$

$\Rightarrow$

$$\frac{\partial \rho(x, y, z, t)}{\partial t} + \frac{\partial}{\partial x} \rho U + \frac{\partial}{\partial y} \rho V + \frac{\partial}{\partial z} \rho W = 0$$

Choose (U, V, W) directions for illustration. Sign takes care of it.

$\frac{kg}{m^3} \frac{m}{s} m^2$

Chain Rule:

$$\frac{\partial \rho}{\partial t} + u \frac{\partial \rho}{\partial x} + v \frac{\partial \rho}{\partial y} + w \frac{\partial \rho}{\partial z} + \rho \frac{\partial u}{\partial x} + \rho \frac{\partial v}{\partial y} + \rho \frac{\partial w}{\partial z} = 0$$

Vector Notation:

$$\frac{\partial \rho}{\partial t} + \underbrace{\vec{U} \cdot \vec{\nabla} \rho}_{\text{Rate of change of } \rho \text{ at } x, y, z} + \rho \underbrace{\vec{\nabla} \cdot \vec{U}}_{\text{Divergence of } \vec{U}} = 0$$

Example

Using

$$\frac{D\rho}{Dt} = \left(\frac{\partial}{\partial t} + \vec{U} \cdot \vec{\nabla} \right) \rho = -\rho \vec{\nabla} \cdot \vec{U}$$

↳ Rate of change of density along air parcel

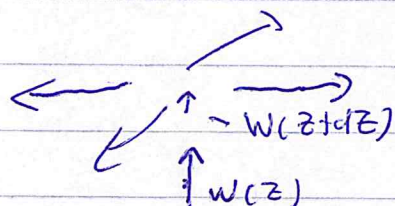
Change of density in a moving $\vec{U}$ parcel is due to divergence. $\vec{\nabla} \cdot \vec{U} > 0$ divergence, flow out, $\Rightarrow$

$$\frac{D\rho}{Dt} < 0$$

Example

If $\rho = \text{constant}$, $\partial \rho / \partial t = 0$ $D\rho = 0$,

$$\vec{\nabla} \cdot \vec{U} = 0 = \frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} + \frac{\partial w}{\partial z}$$

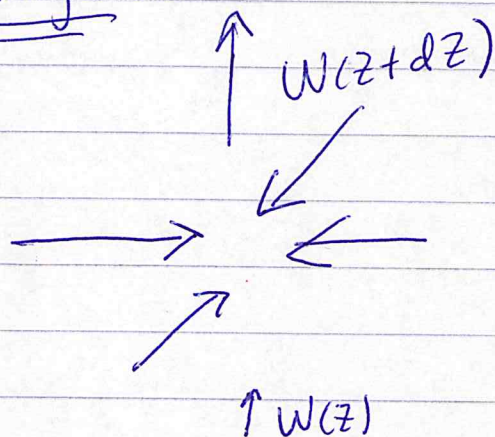


$$\text{Divergence } \frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} > 0$$

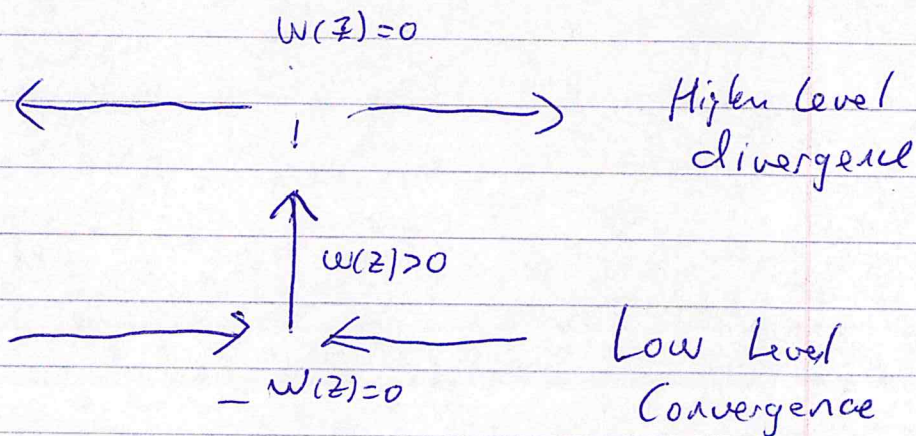
$$\Rightarrow \frac{\partial w}{\partial z} < 0$$

Similarly if $\frac{\partial v}{\partial x} + \frac{\partial v}{\partial y} < 0$, $\frac{\partial w}{\partial z} > 0$

Convergence



Flow must increase in vertical to allow for horizontal convergence



Known as Dines compensation.

Need to combine the continuity Eq with the equation of motion and equation of state to see how the atmosphere works from an analysis perspective.